## Bandwidth enhancement of ground antenna using resonant feeding circuit

## R. Zhang, Y. Liu, H.H. Kim and H. Kim

A loop-type ground antenna with wide-band operation is proposed for USB dongle applications. The solution for improving the bandwidth is based on a resonant feeding circuit that includes both an inductor and a capacitor. By choosing an appropriate ratio of the inductance to the capacitance, the impedance bandwidth (VSWR < 2) is 21.8% at 2.2 GHz, sufficient bandwidth to cover both the WCDMA and WiMax frequency bands.

Introduction: Electrically small antennae have recently begun to receive more attention owing to the ever-growing demand for integration and miniaturisation of mobile products. However, designing an electrically small antenna with a wide impedance bandwidth is difficult because the antenna's dimensions have a significant impact on the impedance bandwidth [1]. An innovative loop-type ground antenna [2], formed by a large loop-type current distribution in the ground plane excited by a loop feed structure, has recently been shown to achieve an acceptable impedance bandwidth of 9.6% at 2.4 GHz. A resonant loopfeeding method for exciting the ground antenna, based on the insertion of a capacitor into the loop feed structure, was studied in [3], allowing an improved bandwidth of 16%. In this Letter, we modify the resonant loop feed structure to improve further the impedance bandwidth of the ground antenna. An inductor is added into the feed structure and the capacitance is reduced to maintain the feeding circuit close to the resonant frequency of the ground antenna. The optimal coupling between the feed and the antenna can then be tuned by adjusting the ratio of the inductance to the capacitance to achieve a well-matched impedance over a wide range of frequencies. The validity is demonstrated via both simulation and experimental results. The antenna design goal in this Letter is to cover both the WCDMA and WiMax communication bands in USB dongles, widely used in laptops for mobile broadband access.

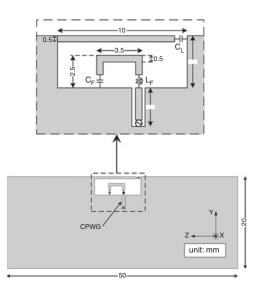


Fig. 1 Structure of proposed antenna

Antenna design and simulated results: Fig. 1 shows the geometry of the proposed antenna structure. The dimensions of the PCB (FR4 substrate,  $\epsilon_r = 4.4$ , tan  $\delta = 0.02$ ) are  $50 \times 20 \times 1$  mm. A  $10 \times 4$  mm clearance is positioned at the centre of the long edge of the PCB. The resonant frequency of the proposed antenna can be controlled by the capacitor C<sub>L</sub>, a phenomenon demonstrated in [2]; its value is chosen to be 0.28 pF. The inductor L<sub>F</sub> and capacitor C<sub>F</sub> are connected in series in a feeding circuit which is further fed through a coplanar waveguide with ground (CPWG). The input impedance can be controlled by either L<sub>F</sub> or C<sub>F</sub>, which changes the mutual impedance between the feeding circuit and the resonant loop formed of C<sub>L</sub>. Furthermore, wide-band impedance matching can be achieved by choosing an appropriate L<sub>F</sub> to C<sub>F</sub> ratio. Fig. 2 shows the variation in the normalised input impedance of the

ground antenna for three different  $L_F$  to  $C_F$  ratios. It is shown that as the ratio increases within the limits, the normalised input impedance of the antenna with  $L_F$  is obviously closer to the 50  $\Omega$  point on the Smith chart and consequently matched over a much wider range of frequencies than an antenna without  $L_F$  (when  $L_F$  is 0 and  $C_F$  is 1 pF). As a result, the optimised  $L_F$  and  $C_F$  values of the proposed antenna are determined to be 11.5 nH and 0.1 pF, respectively.

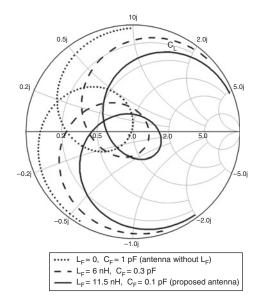


Fig. 2 Smith chart of ground antenna with different  $L_F$  to  $C_F$  ratios

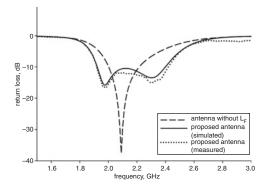
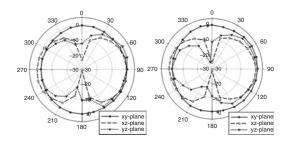


Fig. 3 Simulated and measured return losses



**Fig. 4** Measured radiation patterns of proposed antenna a 1.92 GHz b 2.4 GHz

*Experimental results and discussion:* The return losses of the proposed antenna and the antenna without L<sub>F</sub> are presented in Fig. 3. The simulated and measured results of the proposed antenna are in good agreement. It is noted that two radiation modes occur; one of these is the resonant loop formed of C<sub>L</sub>, which is the same as the antenna without L<sub>F</sub>. The additional mode is generated when the L<sub>F</sub> to C<sub>F</sub> ratio is chosen to be an appropriate value. The impedance bandwidth of the proposed antenna with VSWR < 2 is 480 MHz, a substantial improvement (118%) over the 220 MHz that the antenna without L<sub>F</sub> is capable of, sufficient to cover both the WCDMA and WiMax bands (1.92–2.4 GHz). Fig. 4 plots the measured radiation patterns of the proposed antenna

ELECTRONICS LETTERS 28th March 2013 Vol. 49 No. 7

in the xy, xz and yz planes at both 1.92 and 2.4 GHz. It is apparent that good omnidirectional radiation performance is obtained in the xy plane. The measured radiation efficiency of the proposed antenna from 1.92 to 2.4 GHz is 72% on average, as shown in Fig. 5.

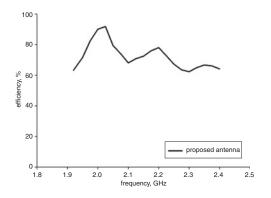


Fig. 5 Measured efficiency of proposed antenna

*Conclusion:* We propose a ground antenna suitable for both WCDMA and WiMax bands (1.92–2.4 GHz) operation in USB dongles. The enhanced impedance bandwidth of the proposed antenna is achieved with a resonant feeding circuit, in which the ratio of the inductance to the capacitance is chosen carefully to match the input impedance of

the antenna over a wide frequency range. The radiation performance of the proposed antenna is verified through experimental results.

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